

ECE 536 – Integrated Optics and Optoelectronics
Lecture 15 – March 8, 2022

Spring 2022

Tu-Th 11:00am-12:20pm

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Lecture 15 Outline

- Amplified Spontaneous Emission (ASE)
- Optical Gain Measurements
- Considerations on Lossy/Gain Media
- Gain Guided Laser
- Index Guided Laser

ASE and Optical Gain Measurements

Experimental Determination of Optical Gain

Measurements of gain continue to be an important component to validate and refine the design of a laser in order to meet desired performance specifications.

Optical stripe-length method

An external laser source is used to excite the sample under investigation. The laser beam is focused as a stripe with a cylindrical lens. The *amplified spontaneous emission* (ASE) is measured as a function of the stripe length and the gain is extracted from a fit of the data. This method is applied to a material which has not yet been processed into a complete laser structure.

Hakki-Paoli method – the laser is operated below threshold. If the length of the device and the facet reflectivity are known, the gain can be evaluated from maxima and minima of the Fabry-Pérot spectrum recorded with a spectrometer of sufficient resolution.

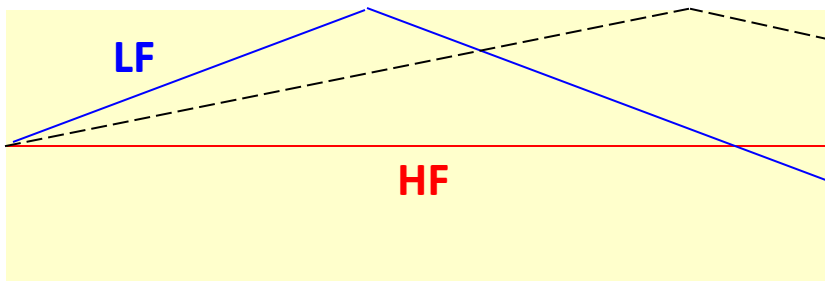
Transmission method – Requires a broadband weak light source, covering the spectral region of interest, transmitted through the device (which should operate in the fundamental mode with suppression of the Fabry-Pérot modes by deposition of anti-reflective coatings on the facets). The amplification of this broadband probe light in the diode is measured and it provides directly the gain spectra.

Review again: effective index n_e

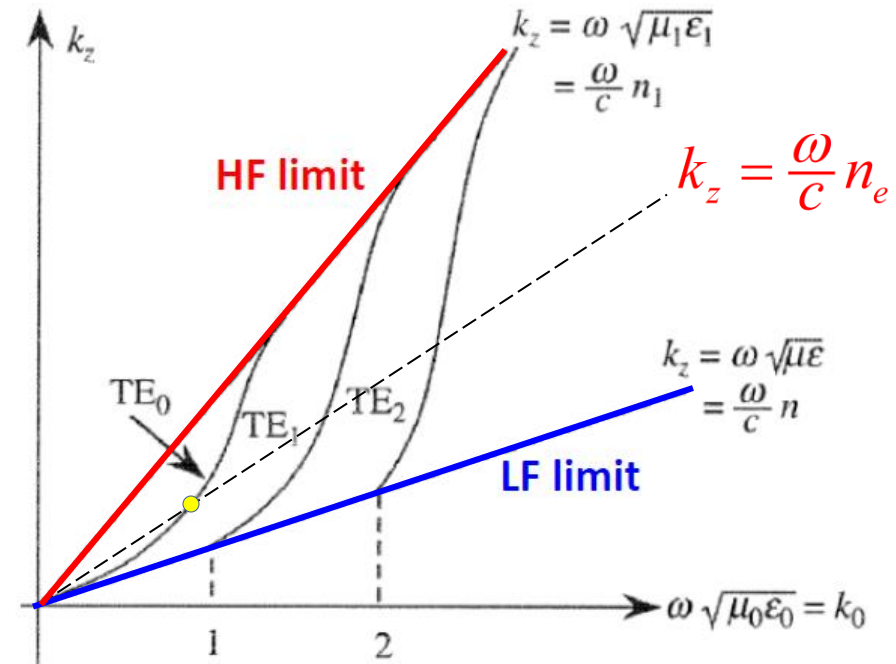
$$k_z = \frac{2\pi}{\lambda_z} = n_e k = n_e \frac{2\pi}{\lambda}$$

$$n_e = \frac{2\pi}{\lambda_z} \frac{\lambda}{2\pi} = \frac{\lambda}{\lambda_z} = \frac{v_p}{f} \frac{f}{v_{pz}} = \frac{v_p}{v_{pz}}$$

$$n < n_e < n_1$$



Strictly, each mode is associated with a specific effective index at a given frequency



Optical Fields in Cavity with Gain

Fabry-Perot Cavity

Initial Field: $E_{sp}(\lambda)$

Field After Single Pass: $E'_{sp}(\lambda) = E_{sp}(\lambda) + E_{sp}(\lambda)r_1r_2e^{i2kL}$

General Expression: $E_{ASE}(\lambda) = E_{sp}(\lambda) \left[1 + r_1r_2e^{i2kL} + (r_1r_2e^{i2kL})^2 + (r_1r_2e^{i2kL})^3 + \dots \right]$

$$\left[1 + a + a^2 + a^3 + \dots \right] = \frac{1}{1 - a}$$



$$E_{ASE}(\lambda) = \frac{E_{sp}(\lambda)}{1 - r_1r_2e^{i2kL}}$$

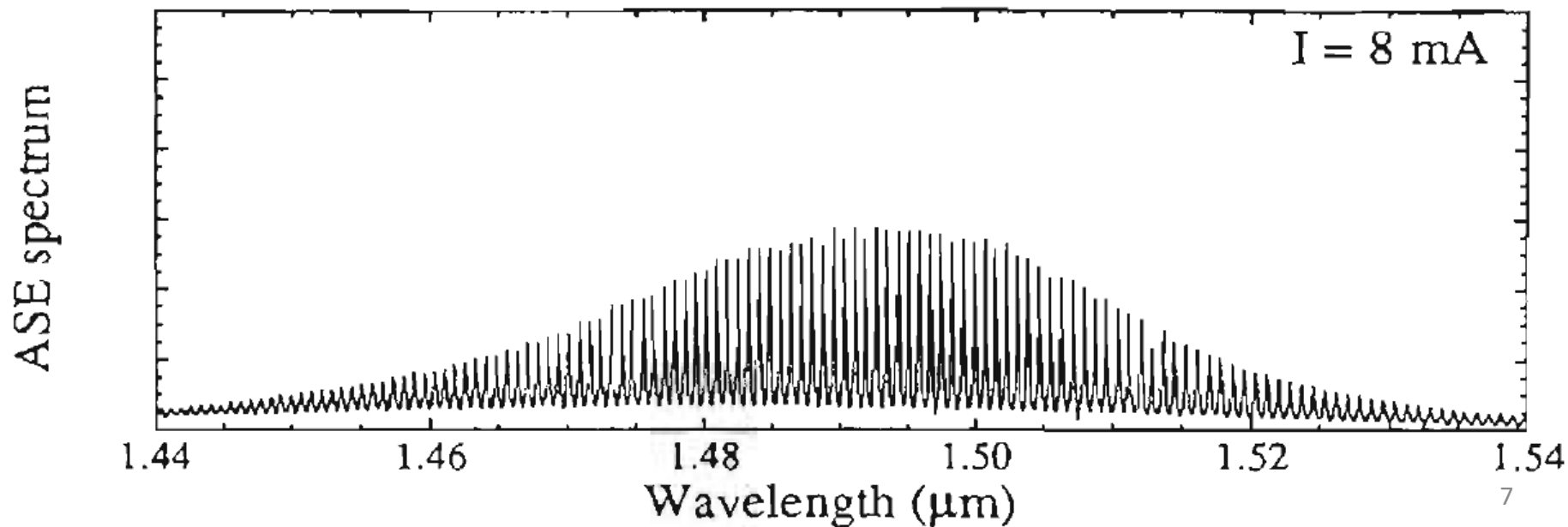
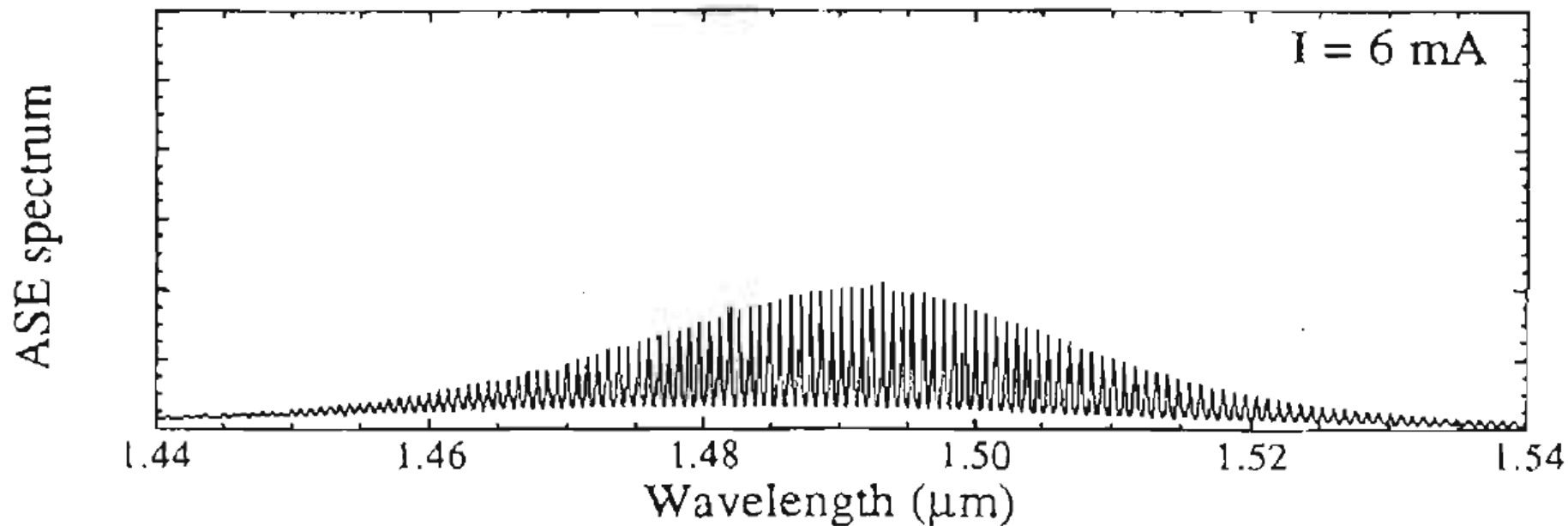
n_e is the effective index

$$k = k' - i\frac{G_n}{2} = \frac{2\pi}{\lambda}n_e - i\frac{G_n}{2}$$

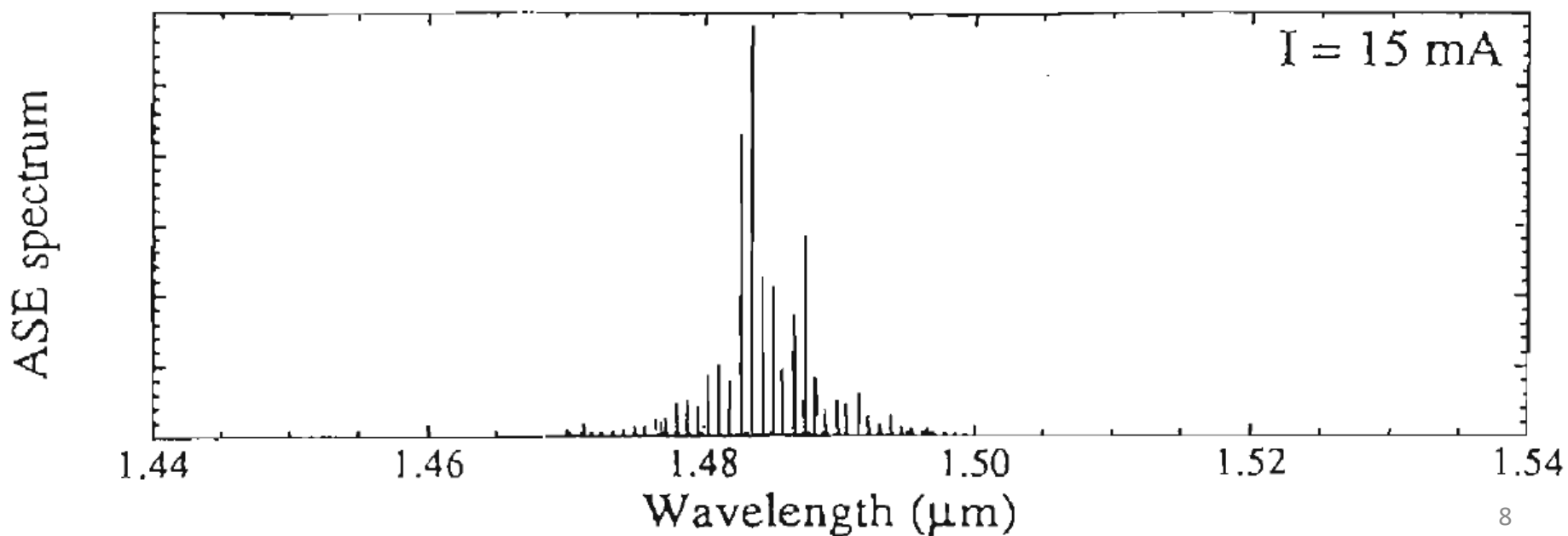
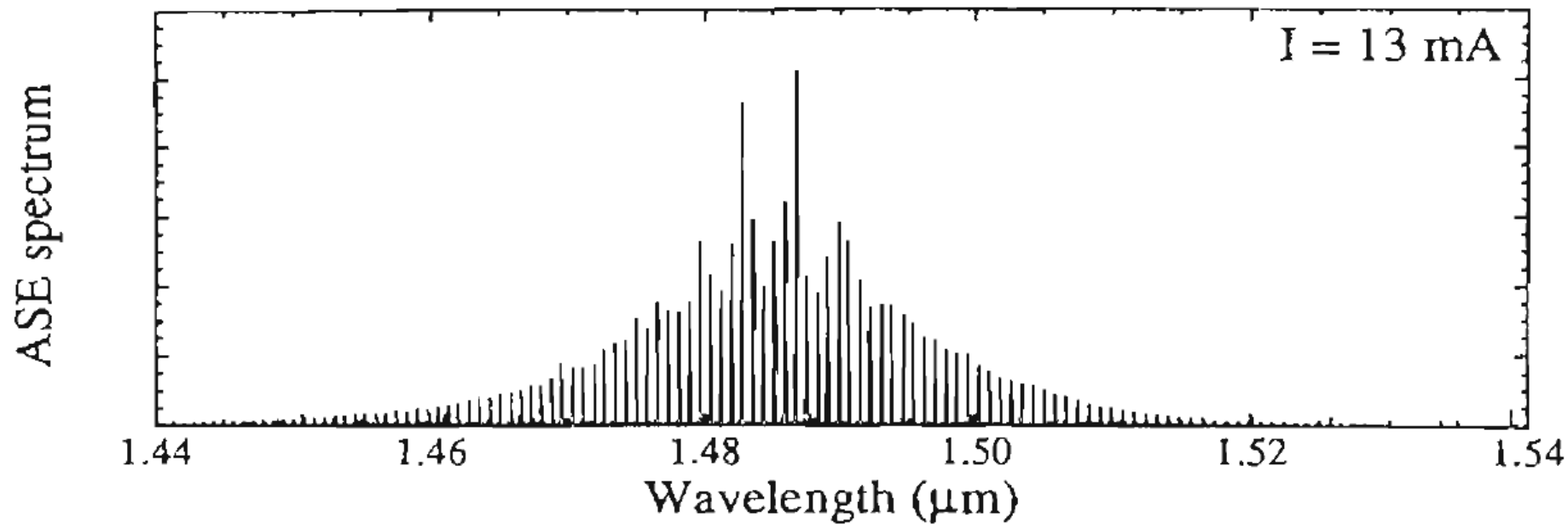
$G_n = \Gamma g - \alpha_i$ is the net modal gain

$$G_n = \Gamma g - \alpha_i$$

ASE Behavior below threshold



ASE Behavior below threshold



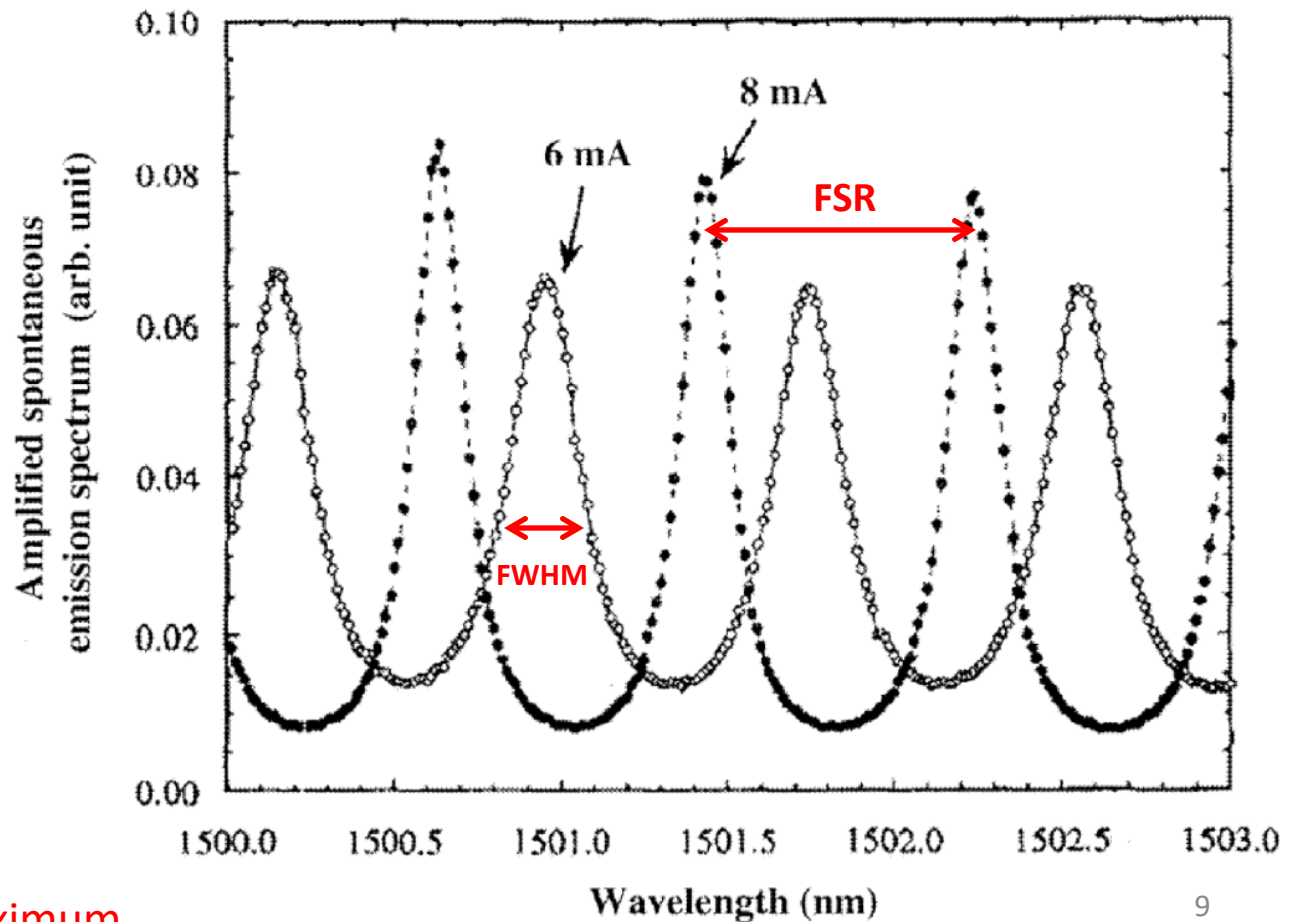
ASE Power Spectrum

$$P(\lambda) \propto |E_{ASE}(\lambda)|^2 = \frac{|E_{sp}(\lambda)|^2}{|1 - r_1 r_2 e^{i2kL}|^2} = \frac{|E_{sp}(\lambda)|^2}{(1 - A)^2 + 4A \sin^2(k'L)}$$

$$A = \sqrt{R_1 R_2} e^{G_n L}$$

$$R_1 = |r_1|^2$$

$$R_2 = |r_2|^2$$



FSR = Free Spectral Range

FWHM = Full Width Half Maximum

Modal Gain from ASE Spectra – 2

Taking the ratio (nearby ASE peaks): $\frac{I_{\max}}{I_{\min}} = \frac{(1+A)^2}{(1-A)^2}$

Solving for A: $A = \frac{\sqrt{I_{\max} / I_{\min}} - 1}{\sqrt{I_{\max} / I_{\min}} + 1} = \sqrt{R_1 R_2} e^{G_n L}$

Solving for G: $G_n = \frac{1}{L} \ln \frac{\sqrt{I_{\max} / I_{\min}} - 1}{\sqrt{I_{\max} / I_{\min}} + 1} + \frac{1}{2L} \ln \frac{1}{R_1 R_2}$

G is the net modal gain.

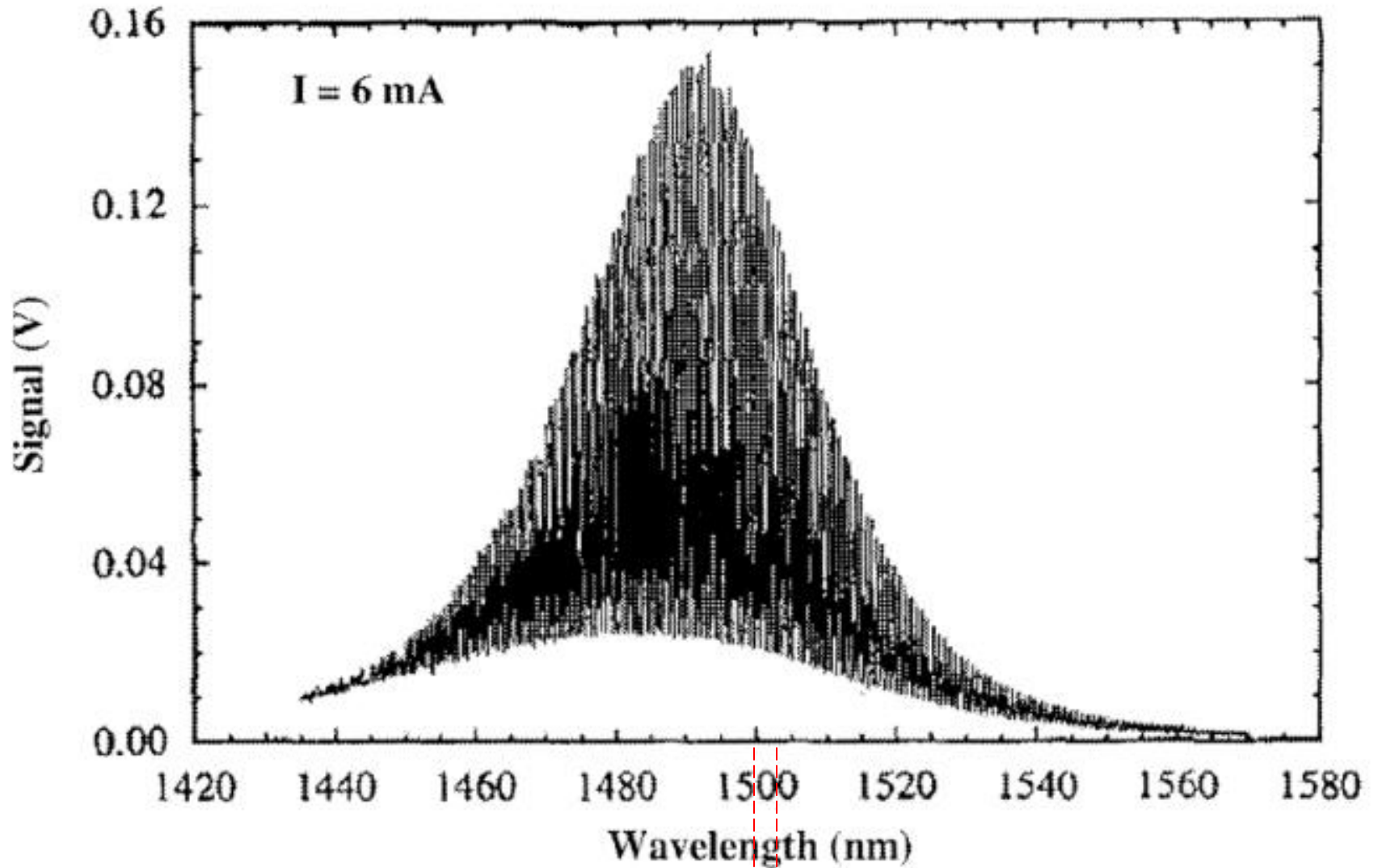
Note: $G_n(\lambda) = \Gamma g(\lambda) - \alpha_i = Q_r + \alpha_m$ where $Q_r = \frac{1}{L} \ln \frac{\sqrt{I_{\max} / I_{\min}} - 1}{\sqrt{I_{\max} / I_{\min}} + 1}$

Hakki-Paoli Method for Gain Measurement

- Measure ASE spectrum
- Take the ratio of the magnitude of I_{max} and I_{min} for the peaks near the m^{th} mode λ_m
- Calculate the mirror reflectivity and either measure the cavity length or calculate it from the measured mode spacing and the effective index n_e
- Gain is calculated using

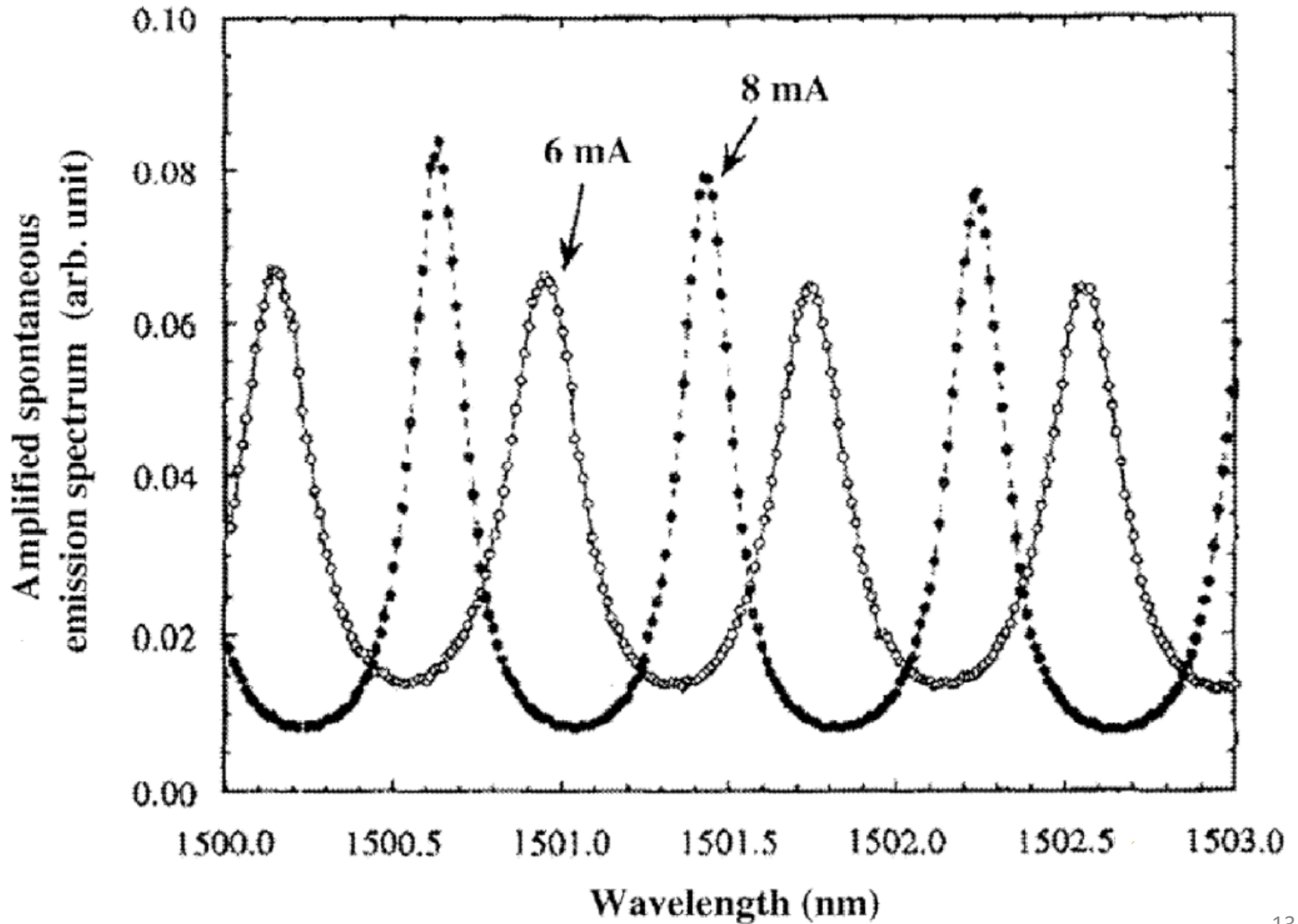
$$G_n(\lambda) = Q_r + \alpha_m$$

Hakki-Paoli Method for Gain Measurement



spectrum range enlarged in next slide

Hakki-Paoli Method for Gain Measurement



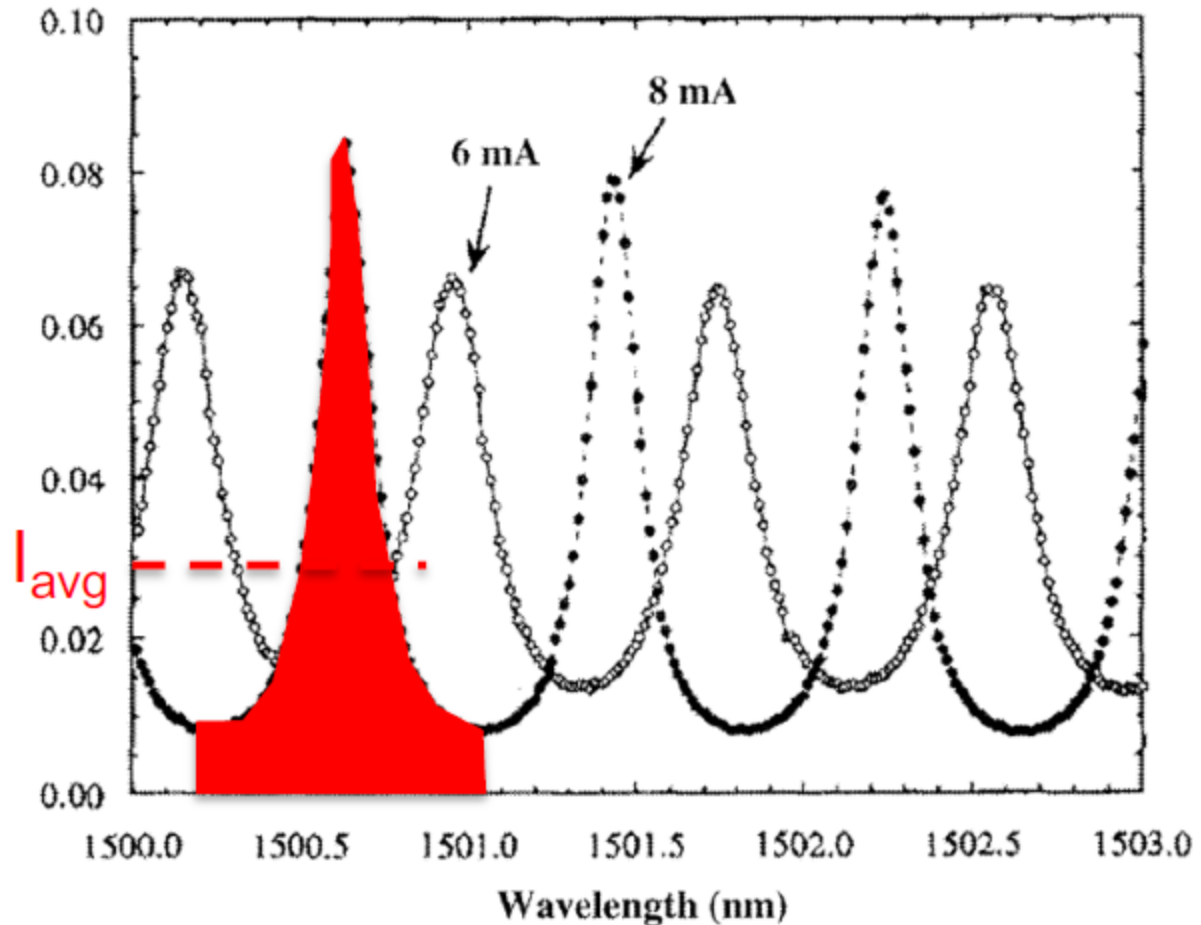
Cassidy's Method – Variant of Hakki-Paoli Method

Based on the Hakki-Paoli method, except that the ratio: I_{avg} / I_{min} is computed.

$$I_{avg} = \sqrt{I_{max} \cdot I_{min}}$$

I_{avg} is more accurate to measure than I_{max} which depends on resolution of the instrument.

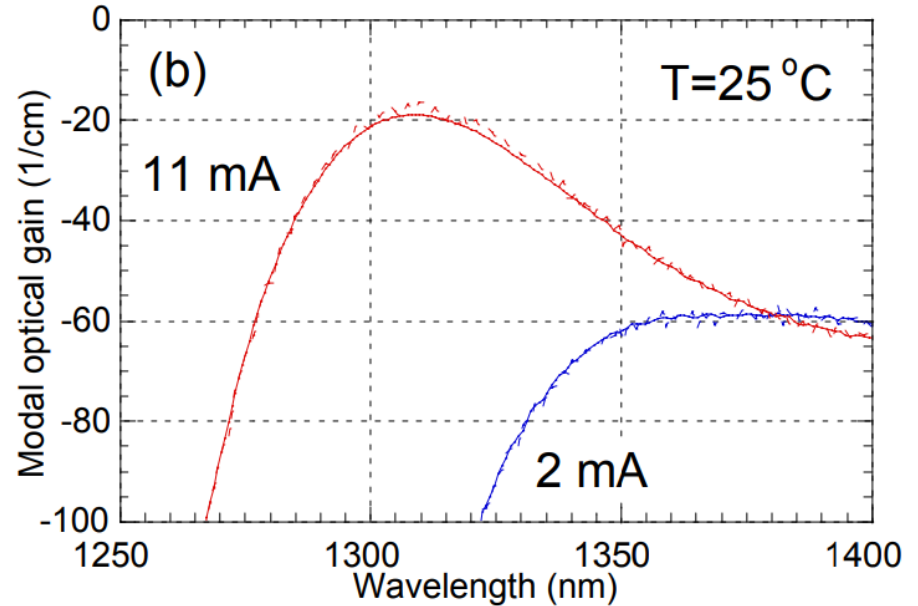
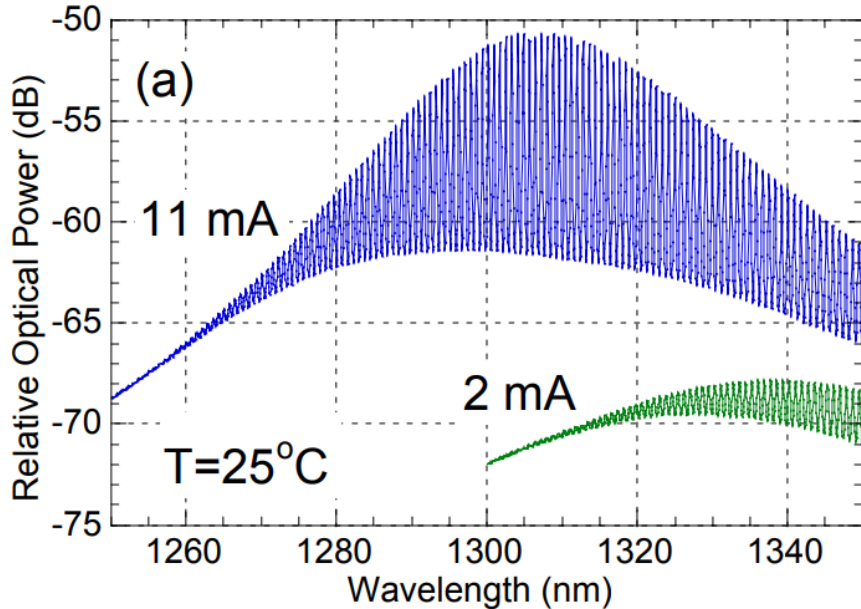
In alternative one can use instead I_{max}/I_{avg} if data is noisy or I_{max} is more accurate than I_{min} .



JAP **56**, 3096 (1984)

JQE **41**, 532 (2005)

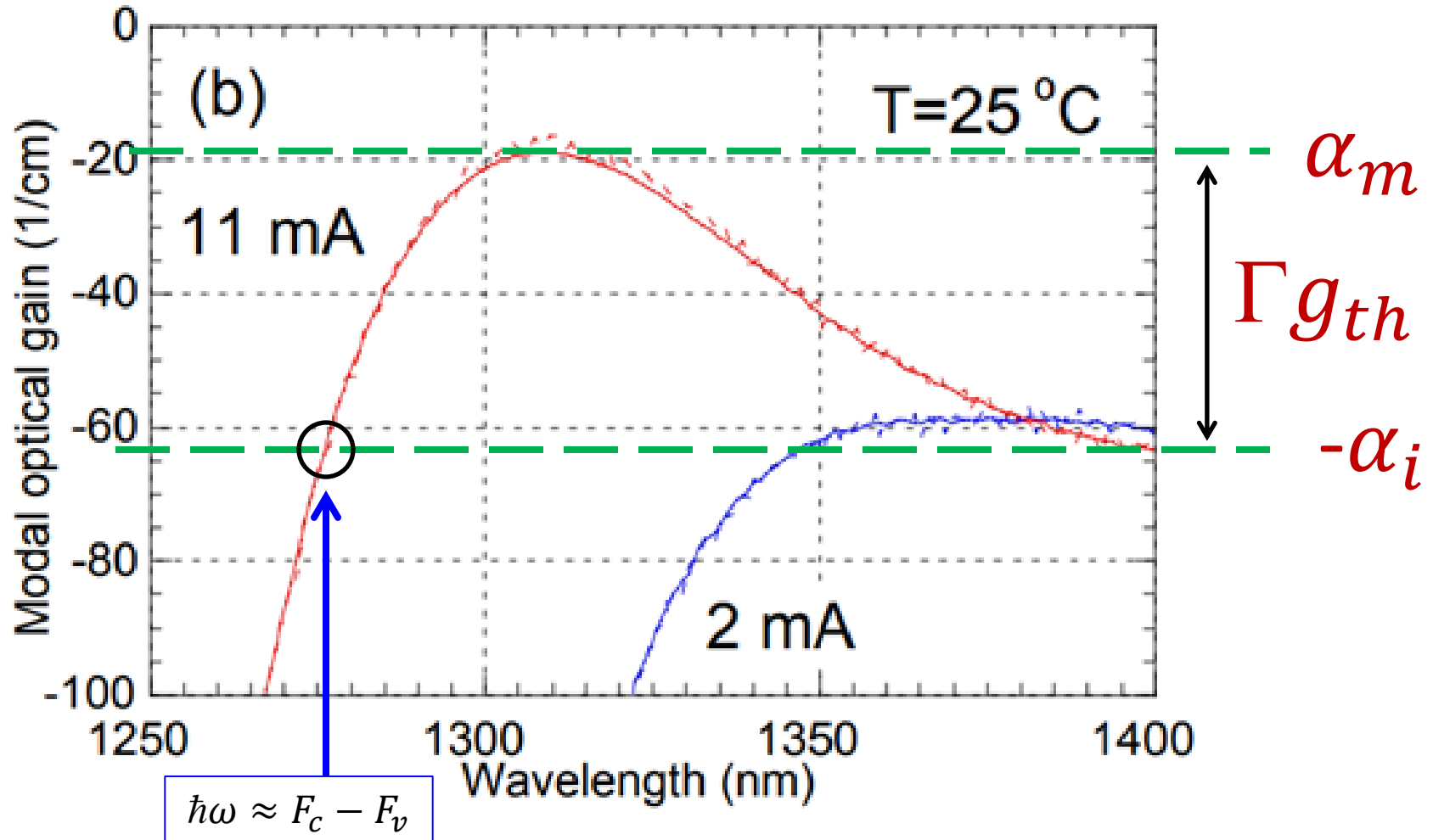
Example



Left: ASE spectra for a $1.3\ \mu\text{m}$ laser with a bulk active region and uncoated mirror facets

Right: Modal optical gain measurements with Hakki-Paoli method (continuous lines) and with Cassidy method (dotted lines)

Characteristics of the G-λ Plot



Below band edge (longer wavelengths) gain is negligible and the plot $G_n(\lambda)$ approaches $-\alpha_i$. The peak occurs at the laser threshold gain $G_n(\lambda) = \Gamma g_{th} - \alpha_i = \alpha_m$.

Lossy Media Waveguides

Waveguide Realized with Lossy Media

In a material with loss or gain, the permittivity is complex

$$\boxed{\varepsilon = \varepsilon' + i\varepsilon''}$$

$$\begin{cases} \varepsilon'' > 0 & \text{loss} \\ \varepsilon'' < 0 & \text{gain} \end{cases}$$

Propagation constant

$$\boxed{k = \omega \sqrt{\mu(\varepsilon' + i\varepsilon'')} = \frac{\omega}{c}(n + i\kappa) = k' + ik''}$$

Consider a waveguide with complex permittivity everywhere

cladding	$\varepsilon' + i\varepsilon''$	$\varepsilon'' > 0$ loss
core	$\varepsilon'_1 + i\varepsilon''_1$	$\varepsilon''_1 < 0$ gain
cladding	$\varepsilon' + i\varepsilon''$	$\varepsilon'' > 0$ loss

Gain Region (core)

expand $\sqrt{\quad}$ assuming $\varepsilon_1'' \ll \varepsilon_1'$

$$k_1 = \omega \sqrt{\mu(\varepsilon_1' + i\varepsilon_1'')} = \omega \sqrt{\mu\varepsilon_1'} \sqrt{1 + i \frac{\varepsilon_1''}{\varepsilon_1'}} \approx \omega \sqrt{\mu\varepsilon_1'} \left(1 + i \frac{\varepsilon_1''}{2\varepsilon_1'} \right) = k_1' - i \frac{g}{2}$$

$$k_1' = \omega \sqrt{\mu\varepsilon_1'} = k_0 n_1$$

gain coefficient

$$g = -k_1' \frac{\varepsilon_1''}{\varepsilon_1'} \quad \left[\text{for } \varepsilon_1'' < 0 \right]$$

Loss Region (cladding)

$$k = \omega \sqrt{\mu(\varepsilon' + i\varepsilon'')} \approx \omega \sqrt{\mu\varepsilon'} \left(1 + i \frac{\varepsilon''}{2\varepsilon'} \right) = k' + i \frac{\alpha}{2}$$

$$k' = \omega \sqrt{\mu\varepsilon_1'} = k_0 n$$

$$\alpha = k' \frac{\varepsilon''}{\varepsilon'} \quad \left[\text{decay constant} \right]$$

Solution to Wave Equation (TE Mode)

$$\mathbf{E} = \hat{y}E_y = \hat{y} \phi(x) e^{ik_z z}$$

$$\left[\frac{d^2}{dx^2} - k_z^2 + \omega^2 \mu \varepsilon(x) \right] \phi(x) = 0$$

We can solve with the variational method to find k_z

$$k_z^2 = \frac{\int_{-\infty}^{\infty} \phi^*(x) \left[\frac{d^2}{dx^2} + \omega^2 \mu \varepsilon(x) \right] \phi(x) dx}{\int_{-\infty}^{\infty} \phi^*(x) \phi(x) dx}$$

$$\varepsilon(x) = \varepsilon^{(0)}(x) + \Delta\varepsilon(x) = \begin{cases} \varepsilon_1' + i\varepsilon_1'' & \text{core} \\ \varepsilon' + i\varepsilon'' & \text{cladding} \end{cases}$$

treat as perturbation

Equation for the unperturbed case (lossless waveguide)

$$\left[\frac{d^2}{dx^2} - k_z^{(0)2} + \omega^2 \mu \epsilon(x) \right] \phi^{(0)}(x) = 0$$

Solving for k_z using unperturbed wave envelopes

$$k_z^2 = k_z^{(0)2} + i\omega^2 \mu \epsilon_1'' \Gamma + i\omega^2 \mu \epsilon'' (1 - \Gamma)$$

with
$$\Gamma = \frac{\int_{\text{inside}} |\phi^{(0)}(x)|^2 dx}{\int_{-\infty}^{\infty} |\phi^{(0)}(x)|^2 dx}$$

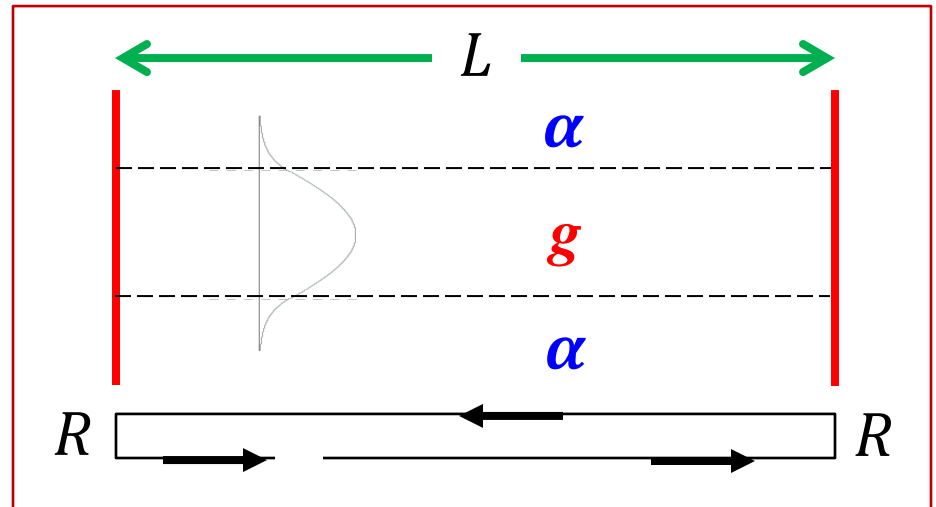
Phase and Threshold Gain Conditions (case $\varepsilon'_1 \sim \varepsilon'$)

$$k_z = \sqrt{k_z^{(0)2} + i\omega^2 \mu \varepsilon_1'' \Gamma + i\omega^2 \mu \varepsilon'' (1 - \Gamma)}$$

$$\simeq k_z^{(0)} - i\Gamma \frac{g}{2} + i(1 - \Gamma) \frac{\alpha}{2}$$

Consider a laser cavity with field reflectivity r and length L

$$r^2 e^{ik_z 2L} = 1$$



$$r^2 e^{i\left(k_z^{(0)} - i\Gamma \frac{g}{2} + i(1 - \Gamma) \frac{\alpha}{2}\right) 2L} = R \cdot e^{i2k_z^{(0)}L} e^{\Gamma g L - (1 - \Gamma)\alpha L} = 1$$

$$r^2 e^{i\left(k_z^{(0)} - i\Gamma\frac{g}{2} + i(1-\Gamma)\frac{\alpha}{2}\right)2L} = R \cdot e^{i2k_z^{(0)}L} e^{\Gamma gL - (1-\Gamma)\alpha L} = 1$$



Phase condition

$$2k_z^{(0)}L = 2m\pi$$

$$k_z^{(0)} \simeq \frac{\omega}{c} n_e$$

Threshold Gain Condition

$$R \cdot e^{\Gamma gL - (1-\Gamma)\alpha L} = 1 \quad \Rightarrow \quad \Gamma g = (1-\Gamma)\alpha + \frac{1}{L} \ln \frac{1}{R}$$

Fabry-Pérot Mode Spacing

$$\left. \begin{aligned} 2k_z^{(0)}L &= 2m\pi \\ k_z^{(0)} &\simeq \frac{\omega}{c}n_e \end{aligned} \right\} \Rightarrow \frac{\omega}{c}n_eL = \frac{2\pi f_m}{c}n_eL = m\pi$$

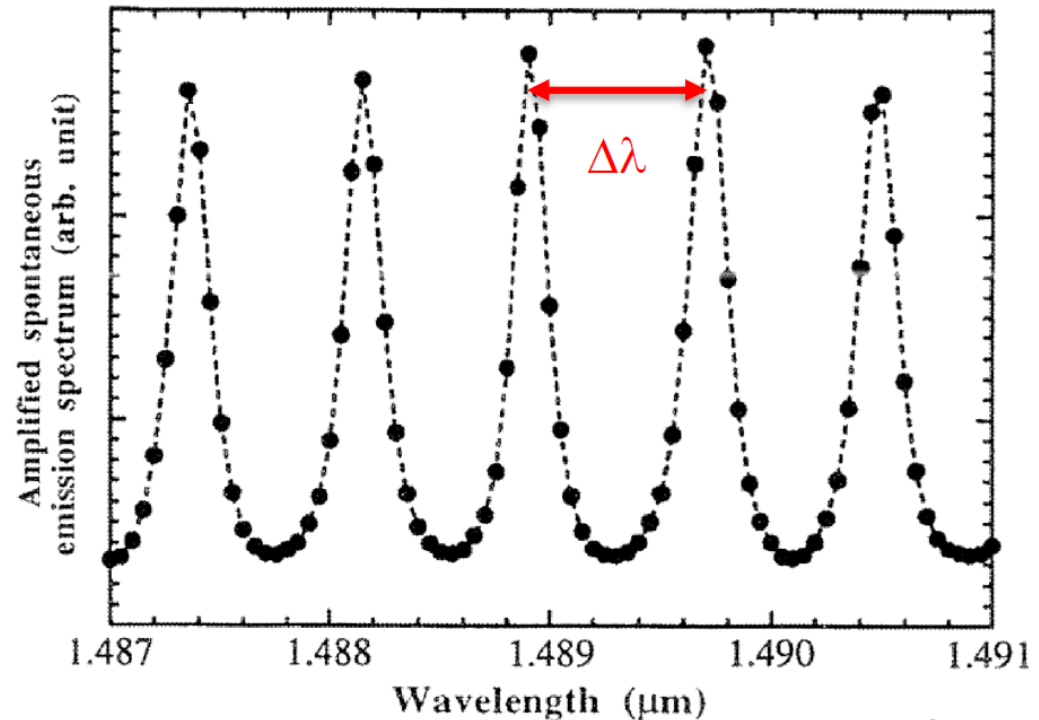
Frequency Spectrum

$$f_m = m \frac{c}{2n_eL}$$

Fabry-Pérot Frequency Spacing

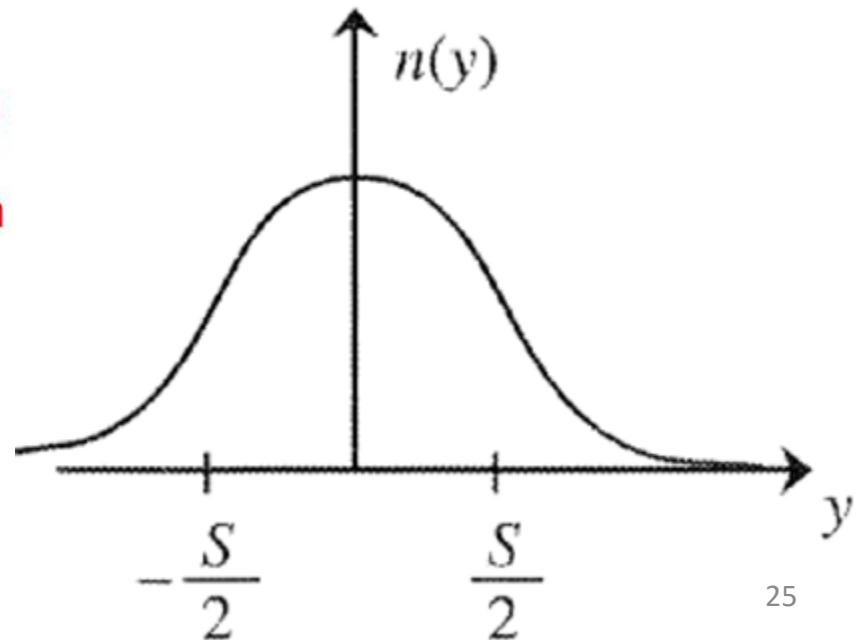
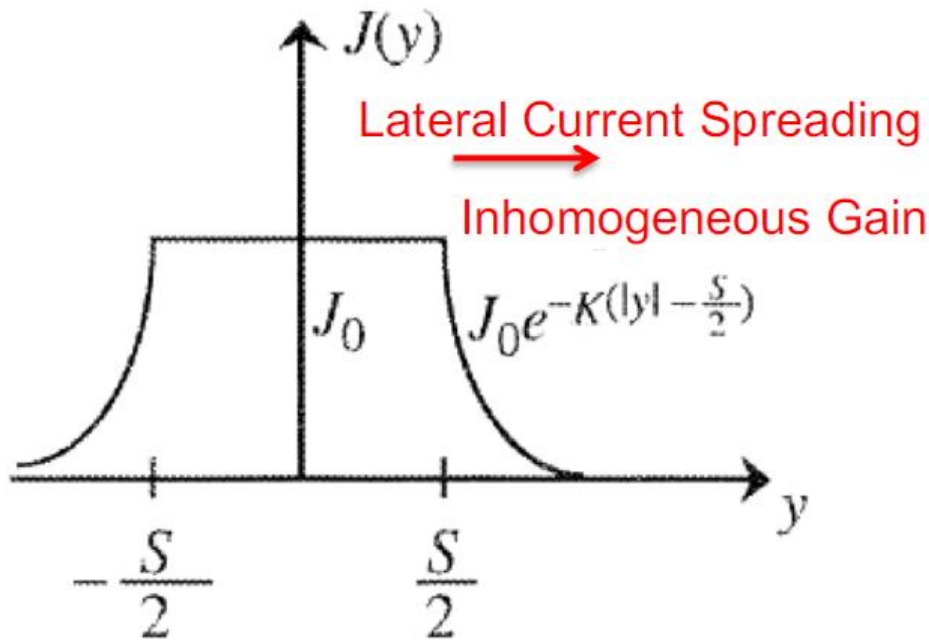
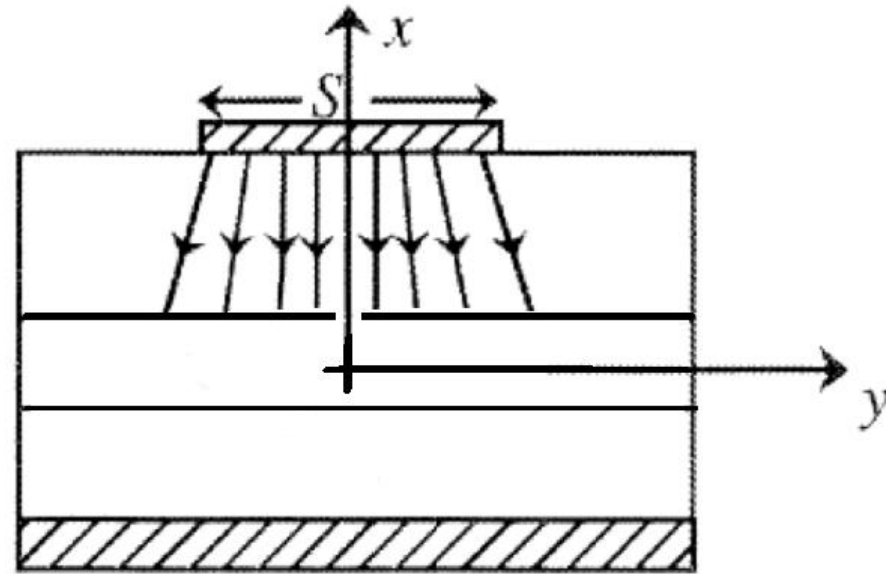
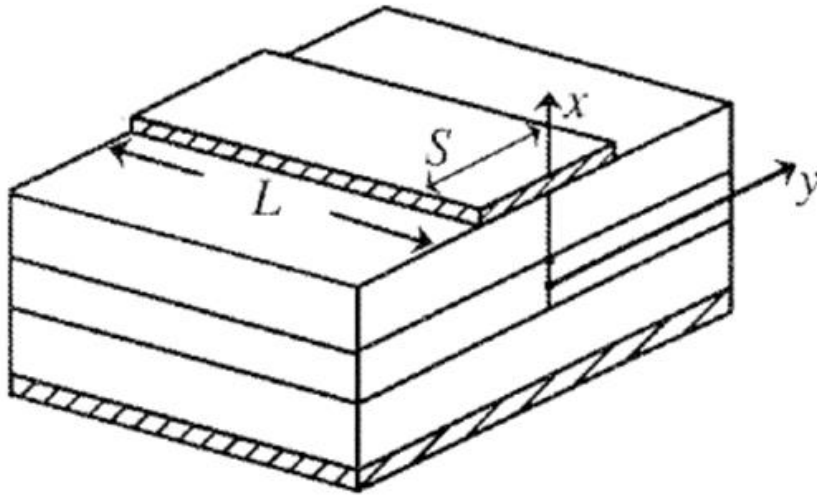
$$\Delta f = \frac{c}{2n_gL} \equiv FSR$$

Free spectral range (FSR)



Gain-Guided Lasers

Stripe-Geometry Laser



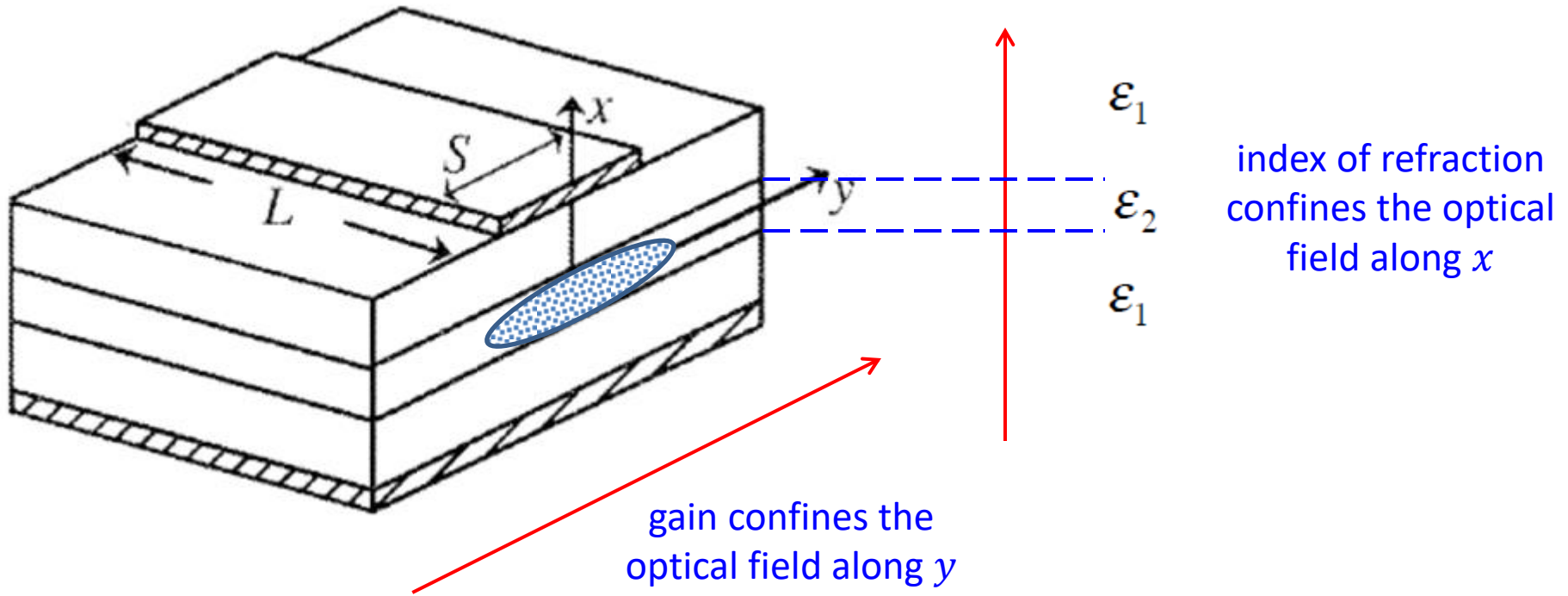
Gain-Guided Lasers

Gain guided lasers have no internal lateral structure. The sole lateral variation along y is the charge density distribution caused by current flow from the conducting stripe and the lateral carrier diffusion within the active region.

At threshold, charge density is maximum beneath the stripe center, hence, most light is generated at the center where gain is greatest. For this reason the light is said to be gain guided.

In such a structure without lateral confinement, light tends to “leak” radially. Additionally, the charge within the active region acts to depress the real refractive index at the lasing frequency further enhancing the lateral radiation losses. There is competition between “guiding” and “antiguinding”

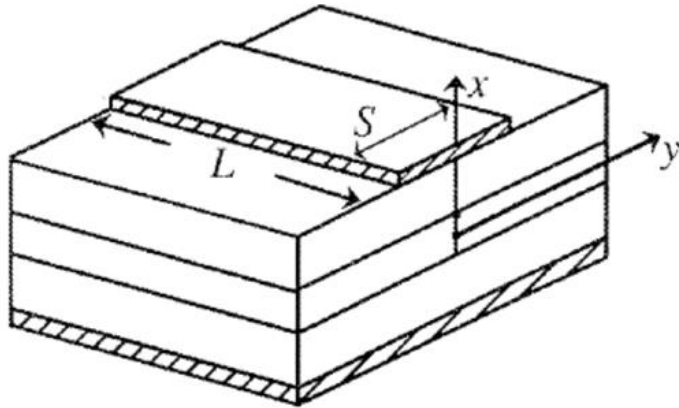
Gain-Guided Lasers



$$\varepsilon(x,y) = \begin{cases} \varepsilon_1 & x > d/2 \\ \varepsilon_2(0) - a^2 y^2 & |x| \leq d/2 \\ \varepsilon_1 & x < -d/2 \end{cases}$$

with $a = a_r + ia_i$ complex

Consider a TE mode in the gain guided laser



Form of the Electric Field

$$\mathbf{E} \approx \hat{y}E_y(x, y, z) \approx \hat{y} \underbrace{F(x)} \underbrace{G(y)} e^{ik_z z}$$

space decomposition

Wave Equation

$$\nabla^2 E_y + \omega^2 \mu \varepsilon(x, y) E_y = 0$$

A solution can be found analytically from perturbation theory in terms of **Hermite polynomials** (see section 3.3 of the textbook)

$$E_y(x, y, z) = \underbrace{E_y^{(0)}(x)}_{\text{unperturbed Electric Field}} H_n \left(\underbrace{\left((k_0 a)^{1/2} \left(\frac{\Gamma}{\varepsilon_0} \right)^{1/4} y \right)}_{\text{with } a = a_r + ia_i \text{ complex}} \right) e^{-k_0 a \left(\frac{\Gamma}{\varepsilon_0} \right)^{1/2} y^2 / 2} e^{ik_z z}$$

and

$$k_z^2 = \beta_z^2 - \left(\omega^2 \mu a^2 \Gamma \right)^{1/2} (2n + 1)$$

Phase Wavefront

$$E_y(x, y, z) = E_y^{(0)}(x) H_n \left((k_0 a)^{1/2} \left(\frac{\Gamma}{\epsilon_0} \right)^{1/4} y \right) \underbrace{e^{-k_0 a \left(\frac{\Gamma}{\epsilon_0} \right)^{1/2} y^2 / 2} e^{i k_z z}}_{\text{Phase Wavefront}}$$

Consider the case $n = 0$

$$k_z^2 = \beta_z^2 - (\omega^2 \mu a^2 \Gamma)^{1/2}$$

$$e^{-k_0 a \left(\frac{\Gamma}{\epsilon_0} \right)^{1/2} y^2 / 2} e^{i k_z z}$$

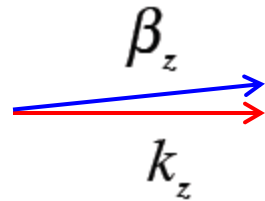
$$a = a_r + i a_i$$

$$k_z \sim \beta_z$$

$$e^{-i a_i k_0 \left(\frac{\Gamma}{\epsilon_0} \right)^{1/2} y^2 / 2}$$

$$e^{i \text{Re}(k_z) z}$$

phase propagators



Phase Wavefront

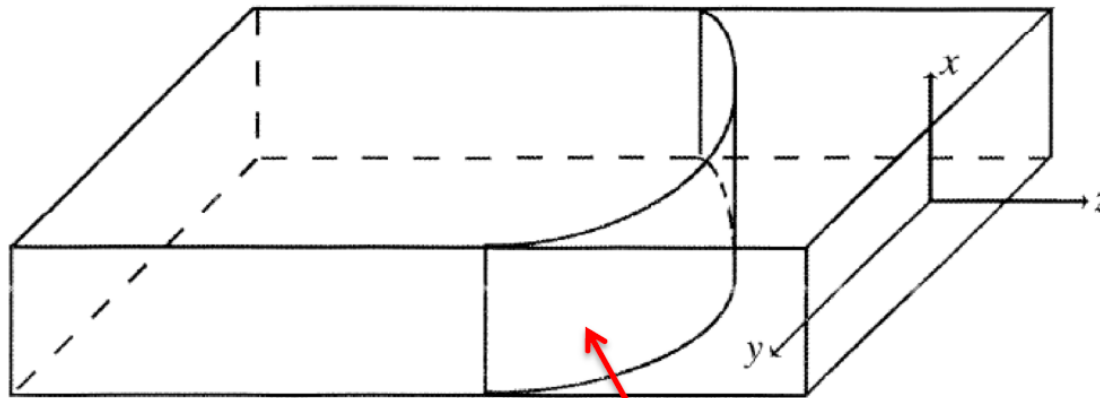
phase propagators

$$e^{-ia_i k_0 \left(\frac{\Gamma}{\epsilon_0}\right)^{1/2} y^2 / 2}$$

$$e^{i \operatorname{Re}(k_z) z}$$

Surface of constant phase (wavefront) occurs where

$$\operatorname{Re}(k_z) z - k_0 a_i \left(\frac{\Gamma}{\epsilon_0}\right)^{1/2} \frac{y^2}{2} = \text{constant}$$



Constant Phase
Surface

(cylindrical parabolic)

Wave vector

$$k_z^2 - \beta_z^2 = -(\omega^2 \mu a^2 \Gamma)^{1/2}$$

$$(k_z + \beta_z)(k_z - \beta_z) = -(\omega^2 \mu a^2 \Gamma)^{1/2}$$

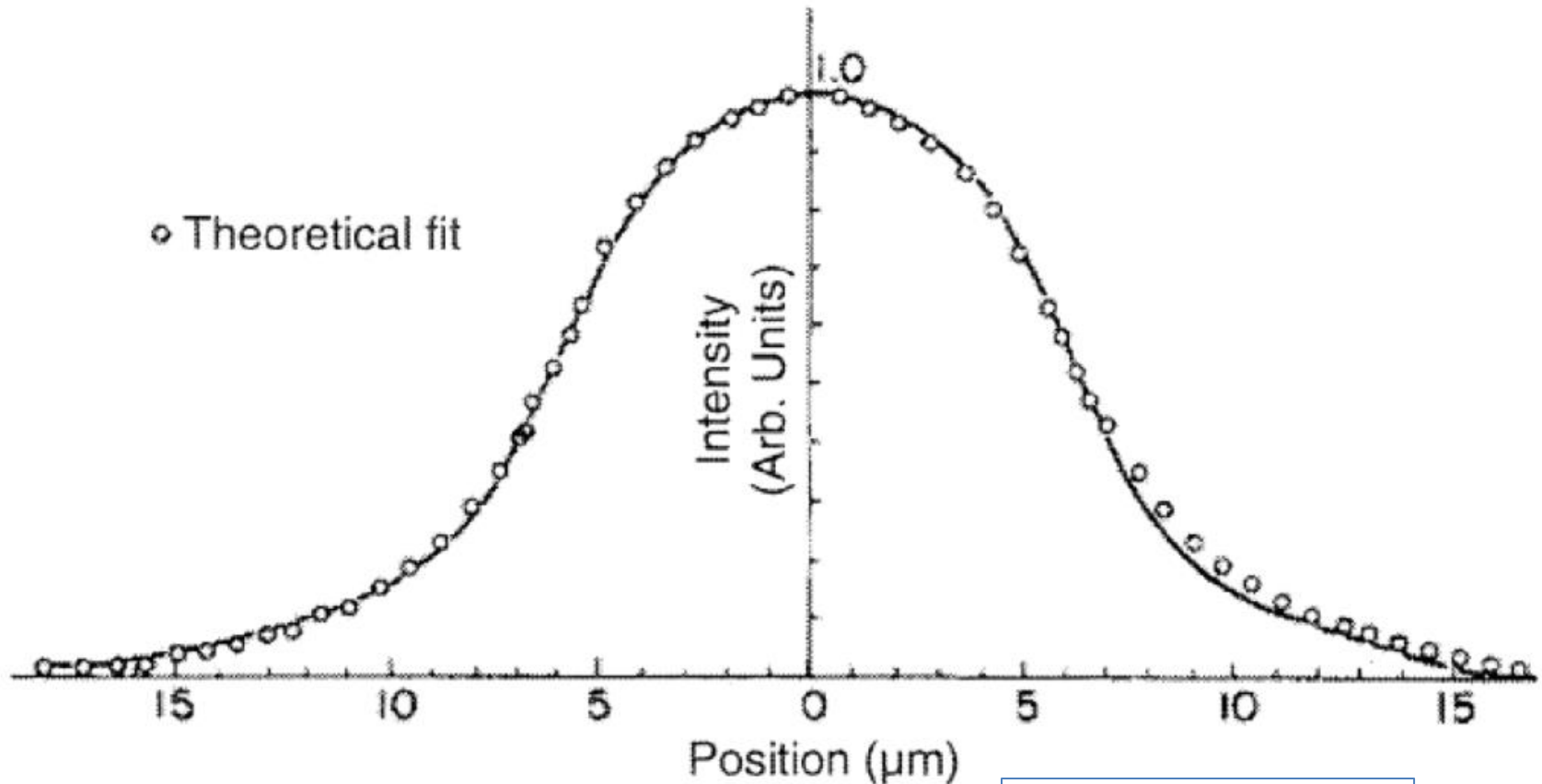
$$k_z \approx \beta_z$$

$$2\beta_z(k_z - \beta_z) \approx -(\omega^2 \mu a^2 \Gamma)^{1/2}$$

$$k_z \approx \beta_z - \frac{1}{2\beta_z}(\omega^2 \mu a^2 \Gamma)^{1/2} = \beta_z - \frac{k_0 a}{2\beta_z} \left(\frac{\Gamma}{\epsilon_0} \right)^{1/2}$$

Carrier Density Profile

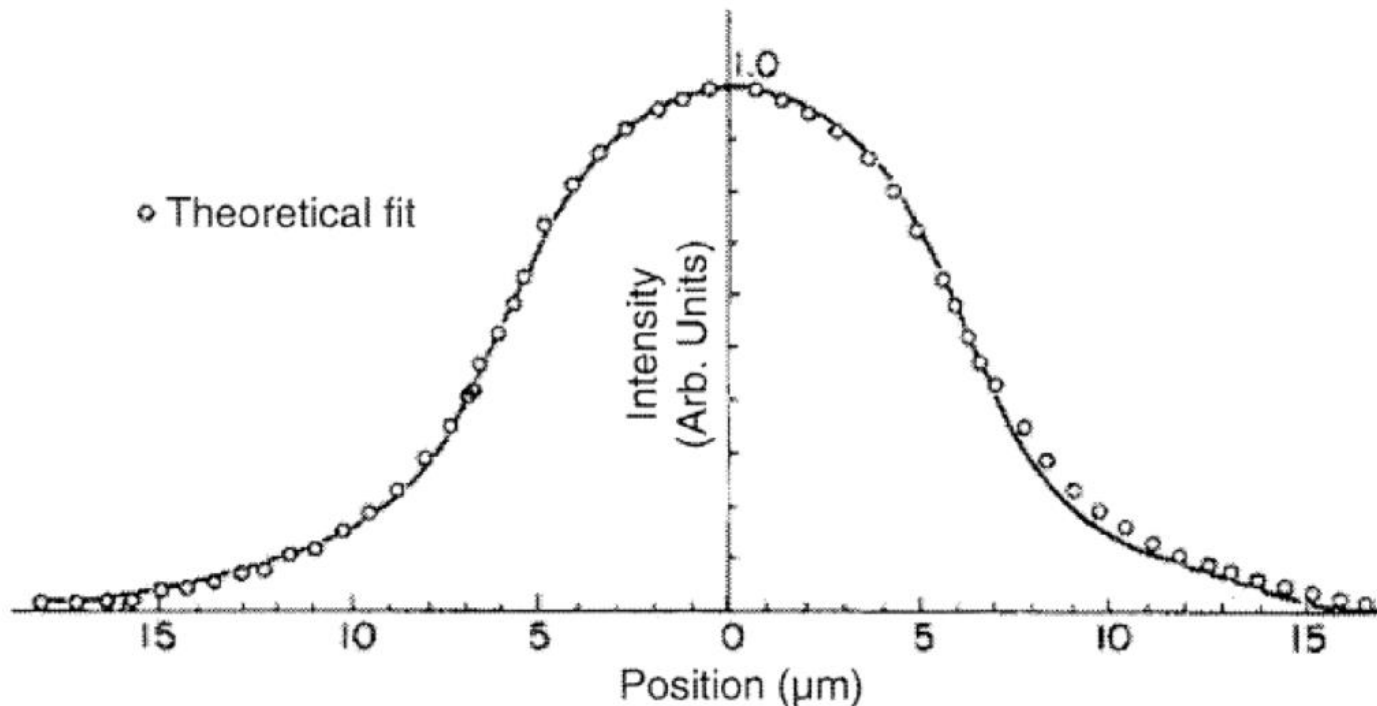
The carrier density may be mapped by measuring the spontaneous emission intensity profile



Carrier Density Profile

If we neglect current spreading down to the depth of the active layer from the stripe contact, a purely diffusive model yields:

$$\delta n(y) = \begin{cases} Ae^{-y/L_n} + Be^{y/L_n} + G_0\tau_n & |y| \leq S/2 \\ Ce^{-\left(|y| - \frac{S}{2}\right)/L_n} & |y| \geq S/2 \end{cases}$$



Index of refraction

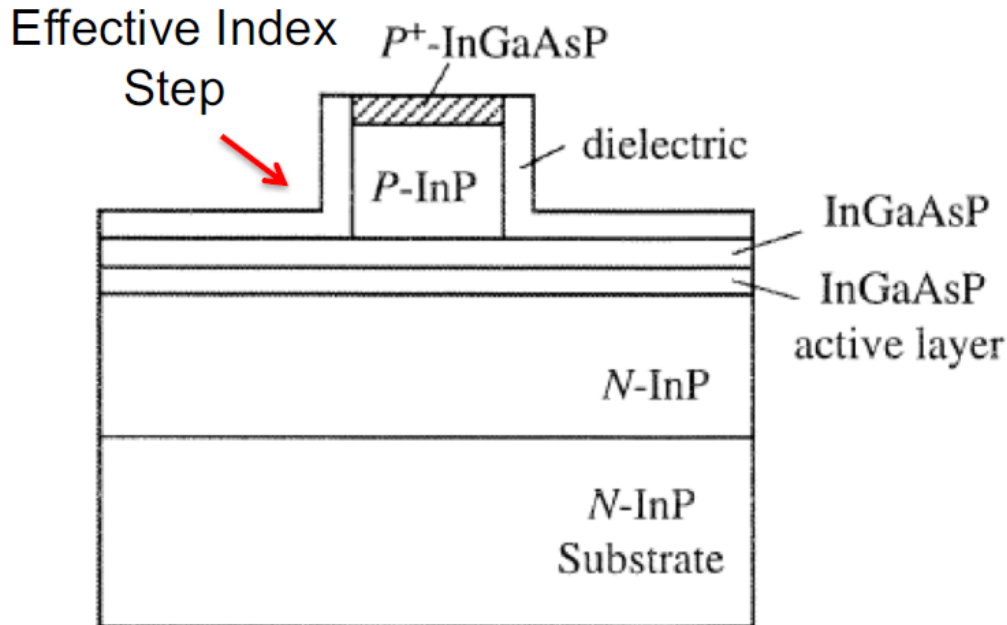
The model obtained for the index of refraction has the form

$$n_r(y) = \left(\frac{\epsilon_{2r}(0)}{\epsilon_0} \right)^{1/2} \left[1 - \frac{a_r^2 - a_i^2}{2\epsilon_{2r}(0)} y^2 \right]$$

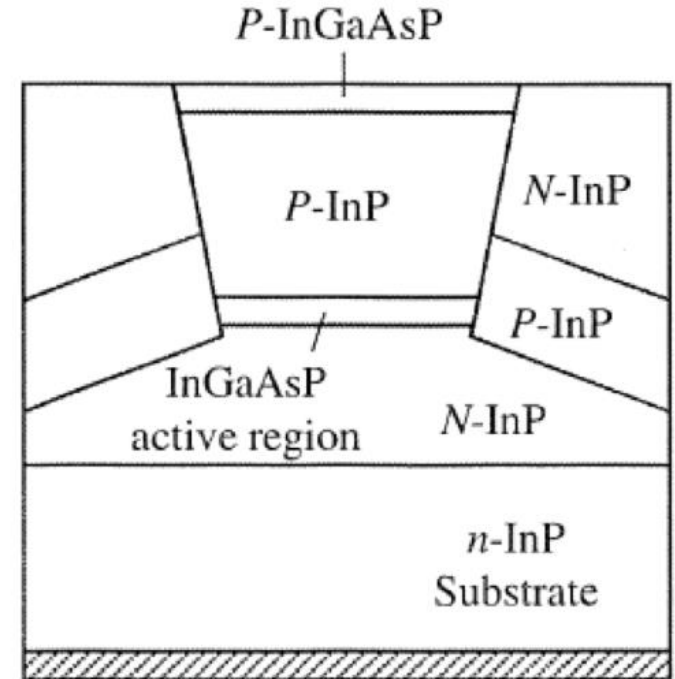
$$n_i(y) = \left(\frac{\epsilon_{2r}(0)}{\epsilon_0} \right)^{1/2} \left[\frac{\epsilon_{2i}(0) - 2a_r a_i y^2}{2\epsilon_{2r}(0)} \right]$$

Index-Guided Lasers

Ridge-Waveguide Laser



Buried Heterostructure



ADVANTAGES:

- Lower threshold current density
- Higher differential quantum efficiency
- Better optical confinement and mode control

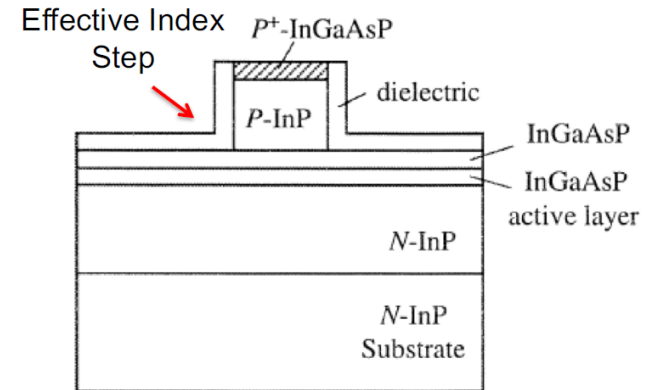
Confinement factor

The effective index can be determined by solving the slab waveguide problem under the ridge and outside the ridge.

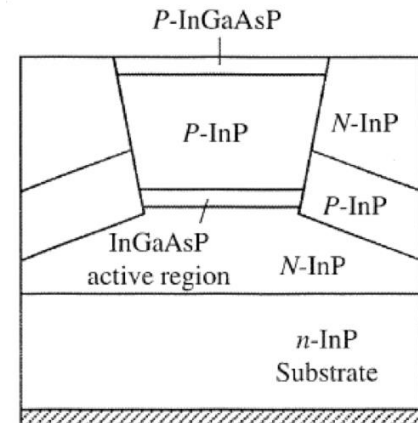
Confinement along y is provided by the effective index step.

Confinement is created by a change of material properties along x and along y .

Ridge-Waveguide Laser



Buried Heterostructure



Confinement factor

$$\mathbf{E} \simeq \hat{y}E_y(x, y, z) \simeq \hat{y}F(x)G(y)e^{ik_z z}$$

Optical Confinement Factor:

$$\Gamma = \frac{\int \int_{\text{active region}} \frac{1}{2} \operatorname{Re}(\mathbf{E} \times \mathbf{H}^*) \cdot \hat{z} \, dx dy}{\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{1}{2} \operatorname{Re}(\mathbf{E} \times \mathbf{H}^*) \cdot \hat{z} \, dx dy}$$

$$\text{using } \frac{1}{2} \operatorname{Re}(\mathbf{E} \times \mathbf{H}^*) \cdot \hat{z} \simeq \frac{1}{2} \operatorname{Re}(-E_y H_x^*) = \frac{k_z |E_y|^2}{2\omega\mu}$$

$$\Gamma = \frac{\int \int_{\text{active region}} |E_y(x, y)|^2 \, dx dy}{\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} |E_y(x, y)|^2 \, dx dy} \simeq \Gamma_x \Gamma_y$$